

BBL	1	OX	GW 679	NET 641
	2	OX	$\frac{663}{1342}$	$\frac{625}{1266}$
	3	SULF.	574	536
	4	SULF.	564	526
	5	SULF.	$\frac{372}{1510}$	$\frac{334}{1396}$

OX .039
 .039
BWS- .055
 .033
 .040
 .030
 .060

 .042

ASSAY RECORDS FROM 8/6/90

7 samples of OX

Footage of 6" core, Top $\geq .020$ remaining

Hole #

INTERVAL length grade Box #

D88-65

(72.8 - 73.7)	.9	.043	52
(79.9 - 80.5)	.6	.075	51
(83.5 - 84)	.5	.051	51
(87 - 88)	1.0	.078	50
(91.4 - 92.1)	.7	.023	50
(95.3 - 95.9)	.6	.041	49
(98.5 - 99)	.5	.045	49
(123.7 - 124)	.3	.061	45
(128 - 128.6)	.6	.023	45
(131.4 - 132)	.6	.120	44
(135.2 - 135.6)	.4	.048	44
(139.1 - 139.8)	.7	.044	43
(142.8 - 143.4)	.6	.116	43
(177.1 - 177.8)	.7	.057	38
(181.5 - 182)	.5	.037	38
(152.6 - 153.1)	.5	.025	41
(161.3 - 161.9)	.3	.053	40
(164.9 - 165.6)	.7	.021	40
(168.4 - 168.7)	.3	.023	39
(102.2 - 102.9)	.7	.051	48
(215.2 - 215.6)	.4	.034	33
(223.4 - 223.8)	.4	.026	32
(227.2 - 228)	.8	.024	32
(253.2 - 253.7)	.5	.053	28
(258.9 - 259.5)	.6	.056	28
(249.9 - 250.3)	.4	.141	29
(262.5 - 263.1)	.6	.046	27
(265.7 - 266.3)	.6	.044	27
(269.6 - 270.2)	.6	.050	26
(273.4 - 274)	.6	.094	26
(322.8 - 323.2)	.4	.039	19
(326.4 - 327.1)	.7	.024	19

18.7' e .051 W.A.G.

.9507

D88-66

(99 - 99.6)	.6	.020	22	*
(95.8 - 96.3)	.5	.041	23	
(91.5 - 92.5)	.9	.044	23	
(80.9 - 81.6)	.7	.054	25	
(87.7 - 88.3)	.6	.034	24	
(192.9 - 193.6)	.7	.021	10	
(189.4 - 189.8)	.4	.027	10	
(185.1 - 185.6)	.4	.062	11	
(237.1 - 238.5)	1.4	.020	4	
(140.8 - 141.4)	.6	.040	17	*
(137.7 - 138.5)	.8	.042	17	*
(214.2 - 215)	.8	.020	7	
(199.9 - 200.7)	.8	.069	9	

42-381 50 SHEETS 3 SQUARE
42-382 100 SHEETS 3 SQUARE
42-383 200 SHEETS 3 SQUARE
NATIONAL

Hole #	Interval	Length	Grade	Box #	
D88-66	(203.7-204.9)	.7	.021	8	
	(266.5-267.6)	1.1	.023	1	
	(261.9-262.9)	.5	.027	1	
	(128.3-128.6)	.6	.028	18	*
	(133.7-134.4)	.7	.050	18	*
	(121.1-121.6)	.5	.042	19	
	(153.3-153.6)	.3	.032	15	
	(144.2-145)	.8	.025	16	*
	(148.4-148.8)	.4	.025	16	*
	(95.8-96.3)	.5	.041	23	*
	(91.5-92.5)	1.0	.044	23	*
	(114.2-115)	.8	.045	20	*
	(80.9-81.6)	.7	.054	25	*
	(87.7-88.3)	.6	.037	24	*
	(106.9-107)	.6	.024	21	*
		18.6'	@ .035 W.A.G.		(.6562)
D88-67	(218.9-219.5)	.6	.035	32	
	(226.7-227.6)	.9	.038	31	
	(230.6-231.3)	.7	.108	31	
	(239.3-240.1)	.8	.193	29	
	(243.4-244)	.6	.152	29	
	(296.1-296.8)	.7	.104	22	
	(299.8-301.5)	.7	.237	22	
	(305.1-305.8)	.7	.188	21	
	(310.5-311.5)	1.0	.032	21	
	(277.4-277.8)	.4	.032	25	
	(273.9-274.5)	.6	.051	25	
	(234.8-236)	1.2	.081	30	
	(247.4-248)	.6	.036	30	
	(263.2-264)	.8	.041	27	
	(284-284.7)	.7	.157	24	
	(254.7-255.3)	.6	.094	28	
	(249.7-251.4)	.7	.110	28	
	(162.2-163)	.8	.036	36	
	(214.8-215.3)	.5	.073	33	
	(210.6-211.4)	.8	.058	33	
	(270.2-271)	.8	.053	26	
	(266.7-267.3)	.5	.020	26	
	(169.5-170)	.5	.122	35	
	(165.6-166.2)	.6	.038	35	
	(205.9-207)	1.1	.029	34	
	(346.9-347.5)	.6	.020	17	
	(343.4-344)	.6	.020	17	
	(329.5-330.8)	1.3	.146	19	
	(325.4-326)	.6	.025	19	
	(338.7-339.9)	1.2	.022	18	
(359.6-360.4)	.8	.042	15		

42-381 30 SHEETS 3 SQUARE
 42-382 30 SHEETS 3 SQUARE
 42-383 30 SHEETS 3 SQUARE
 NATIONAL

Hole #	Interval	Length	Grade	Box #	
<u>D88-67</u>	(287.4 - 288)	.6	.085	23	
	(291.7 - 293.4)	.7	.020	23	
	(315.4 - 316.5)	.9	.068	20	
	(407 - 407.6)	.6	.030	10	
	(398.5 - 399.6)	.9	.020	10	
	(392 - 393.4)	1.4	.043	11	
	(389.9 - 390.6)	.7	.026	11	
	(384.8 - 385.3)	.5	.025	12	
	(380.7 - 381.6)	.9	.038	13	
	(376.7 - 377)	.3	.030	13	
	(448.5 - 449)	.5	.020	4	
	(455 - 455.8)	.8	.024	4	
	(458.8 - 459.3)	.5	.053	3	
	(433.8 - 434.8)	.4	.049	6	
	(475.1 - 475.9)	.8	.020	1	
	(426.1 - 426.4)	.3	.027	7	
	(429.8 - 430.5)	.7	.037	7	
	(411.7 - 412.7)	1.0	.020	9	
		35.5' @	.063	W.A.G.	2.227

<u>D88-68</u>	(462.2 - 463)	.8	.055	2
	(465.5 - 466)	.5	.061	2
	(470.1 - 471)	.9	.024	3
	(473.7 - 473.2)	.2	.031	3
	(513.8 - 514.6)	.8	.035	8
	(517.8 - 518.6)	.8	.062	8
	(522.2 - 523)	.8	.049	9
	(527.9 - 529.7)	.8	.086	9
	(561.9 - 562.6)	.7	.110	15
	(565.8 - 566.4)	.6	.584	15
	(558.4 - 559.3)	.9	.060	14
	(501.1 - 501.7)	.6	.043	7
	(505 - 507.7)	2.7	.055	7
	(455.1 - 455.9)	.8	.045	1
	(458.5 - 459)	.5	.044	1
	(578.3 - 579)	.7	.087	17
	(582.1 - 582.7)	.6	.080	17
	(547.6 - 548.7)	1.1	.081	13
	(589.9 - 590.8)	.9	.021	18
	(535.8 - 536.2)	.4	.035	11
	(538.9 - 539.2)	.3	.059	11
	(652.7 - 653.4)	.7	.024	26
	(593.6 - 594.2)	.6	.038	19
	(597.6 - 598.2)	.6	.035	19
	(477.5 - 478.2)	.7	.051	4
	(481.7 - 482.6)	.9	.052	4
	(656.5 - 657)	.5	.043	27
(609.2 - 610)	.8	.043	21	

*
*
*

Hole # Interval Length Grade Box #

D88-68

(605.4 - 606)	.6	.027	20	*
(570.3 - 571.6)	1.3	.088	16	
(573.9 - 575.4)	.5	.086	16	
(543.1 - 544)	.9	.038	12	
(496.2 - 497)	.8	.064	6	
(486.9 - 487.7)	.8	.043	5	
(492 - 493)	1.0	.054	5	
<u>27.1' @ .066 W.A.G.</u>			1.7966	

D88-69

(902.2 - 903)	.8	.051	30	
(781.9 - 782.4)	.5	.095	19	
(790.4 - 790.8)	.4	.071	20	
(794.1 - 794.6)	.5	.073	20	
(786.4 - 787.6)	1.2	.215	20	
(887.3 - 887.5)	.2	.034	29	
(890.7 - 890.9)	.2	.026	29	
(894.5 - 895)	.5	.020	29	
(871.7 - 872)	.3	.039	27	
(726.9 - 727.2)	.3	.034	15	
(857.1 - 857.5)	.4	.120	26	
(861 - 861.8)	.8	.072	26	
(640.1 - 640.6)	.5	.057	7	*
(643.4 - 644.5)	.9	.047	7	*
(577.2 - 577.7)	.5	.105	1	
(583.9 - 584.3)	.4	.020	1	
(598.3 - 598.7)	.5	.026	3	
(603.1 - 603.7)	.6	.046	3	
(607.8 - 608.8)	1.0	.042	4	
(620 - 620.6)	.6	.038	5	
(623.1 - 623.8)	.7	.020	5	
(630 - 630.4)	.4	.069	6	
(635.6 - 637.1)	.5	.290	6	
(587.3 - 587.9)	.6	.033	2	
(590.9 - 591.3)	.4	.025	2	
(661.7 - 662)	.3	.025	9	
(669.1 - 669.6)	.5	.040	9	
(656.3 - 657)	.7	.032	8	*
(675.6 - 676.2)	.6	.034	10	
(760.7 - 761.3)	.6	.071	18	A?
(733 - 733.4)	.4	.022	16	
(737 - 737.2)	.2	.025	16	
(813.6 - 814)	.4	.059	22	
(817.2 - 817.8)	.6	.023	22	
(798.8 - 799.4)	.6	.020	21	
(820.8 - 821.2)	.4	.023	23	
(828.5 - 829)	.5	.031	23	
(769 - 769.5)	.5	.063	18	
<u>20.0' @ .062 W.A.G.</u>			1.2461	



Hole #	Interval	Length	Grade	Box #	*
D88-70	(235.5-236)	.5	.049	24	
	(238.4-238.9)	.5	.032	24	
	(178.9-179.8)	.9	.022	16	*
	(62.3-62.8)	.5	.144	1	*
	(123.8-124.3)	.5	.025	9	*
	(83-83.8)	.8	.054	4	
	(87.2-87.9)	.7	.063	4	
	(105-105.7)	.7	.093	7	*
	(109.5-110)	.5	.027	7	*
	(65-65.1)	.1	.144	2	
	(70-72.3)	2.3	.1053	2	
	(75.8-76.6)	.8	.070	3	
	(79.3-79.9)	.6	.080	3	
	(94.8-95.2)	.4	.064	5	
	(113.6-114.9)	.8	.027	8	*
	(119.3-121)	.7	.027	8	*
	(230.4-231)	.6	.048	23	
	(232.1-232.7)	.6	.035	23	
	(222.5-223.2)	.7	.105	22	
	(226.4-227)	.6	.097	22	
(215-215.7)	.7	.1045	21		
(218.9-219.4)	.5	.042	21		
(137.9-138.8)	.9	.021	11	*	
		15.9'	@ .053 W.A.G.		.835

D88-72	(993.9-994)	.1	.029	16	
	(1002.4-1002.9)	.5	.022	16	
	(613.5-614.1)	.6	.021	5	
	(617.2-618)	.8	.027	5	
	(783-783.8)	.8	.024	5	
	(506.4-507)	.6	.021	4	
	(603-603.3)	.3	.025	4	
	(606.1-606.6)	.5	.046	4	
	(610-610.3)	.3	.059	4	
	(787.3-787.7)	.4	.048	6	
	(808.7-809)	.3	.063	7	
	(811.8-812.1)	.3	.067	7	
	(501.3-501.7)	.4	.025	3	
	(821.6-822)	.4	.020	8	
	(303.4-303.9)	.5	.054	1	
	(307.2-307.7)	.5	.044	1	
	(310.8-311.2)	.4	.060	1	
	(837.8-838)	.2	.027	9	
	(841.5-842)	.5	.042	10	
	(845.1-845.2)	.1	.020	10	
	(848.9-849.5)	.6	.021	10	
	(989-989.5)	.5	.032	15	
	(969.1-969.8)	.7	.025	14	
	(972.6-973.7)	1.1	.039	14	
	(976.7-977)	.3	.029	14	
		11.7'	@ .025 W.A.G.		.4145

July 19, 1990

NEED BY 8/10/90

Mr. Micheal P. Attaway
Brohm Mining Corporation
P. O. Box 485
Deadwood, SD 57732

Re: Testing and Evaluating High Pressure Grinding Roll (HPGR)

Dear Mr. Attaway:

The following needs to be done to test and evaluate the use of a HPGR on the sulfide ore (milling) and the oxide ore (heap leaching).

Obtain >1320 pounds of sulfide sample and >1020 pounds of oxide sample. Blend and split out 820 lbs of sulfide ore and 820 lbs of the oxide ore for shipment to West Germany. Retain the remaining portion for comparative testing. The costs for testing are fairly expensive and so I'd suggest one composite sample representing the "average" of each ore. If these results look enticing, then a range of samples can be tested later. Attempt to replicate the makeup of the composite sulfide sample that Hazen Research used for most of their process development so that there is a basis for comparing the metallurgy of HPGR crushed ore with ore crushed the way Hazen did it. The crush size of the sample should be 100% minus 2".

Brohm will need to specify the average % moisture to be expected in both sulfide and oxide ores and the range of moisture to be encountered. Moisture has a significant effect on the HPGR's capacity and the consumption of wear steel.

} NO NEED TO
DO NOW
(8/8/90 JNB
conv. w/ P.C.)

Drum the samples and include a copy of the sample's description and source and the name of the Brohm contact. Request the return of the samples by air freight. Ship the drums to:

KRUPP POLYSIUS A.G.
Research Center
D-4722 ENNIGERLOH
KALKOFEN,
West Germany

ATTN: DEPT. 300, DR. D. KUPPER & DEPT 132, PR. O. OTTE

- LETTER TO OTTE